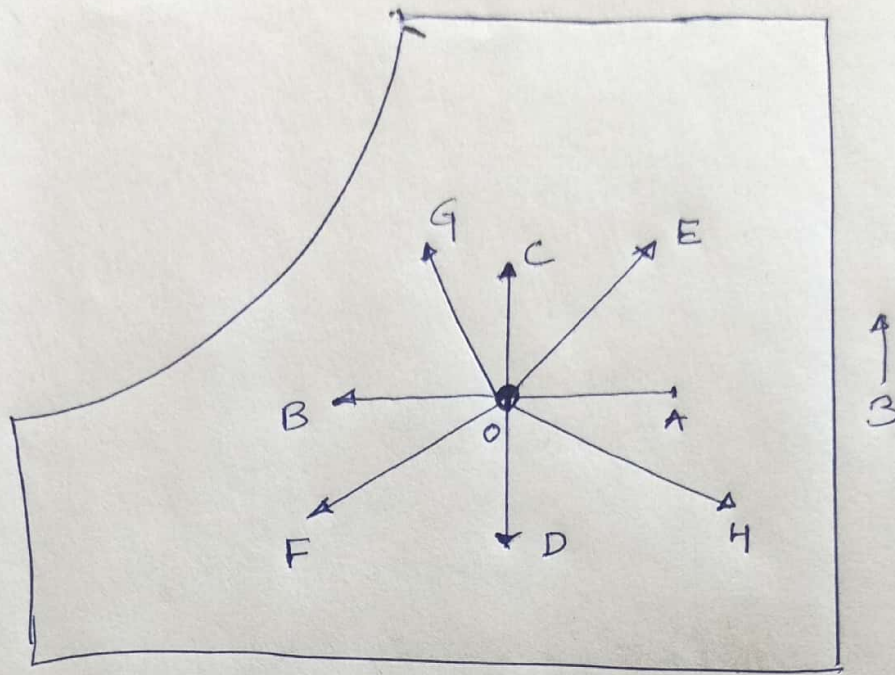
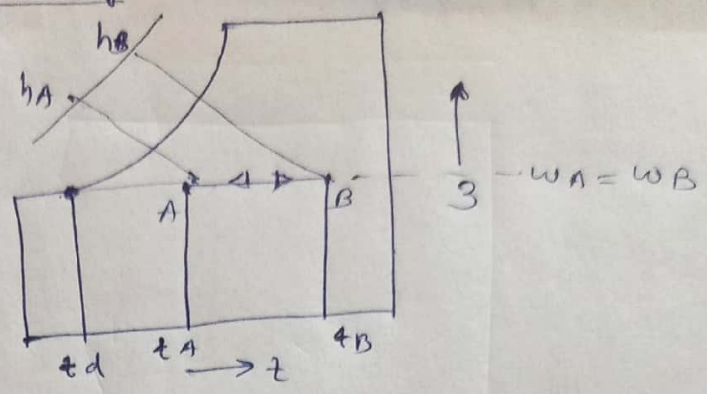


Air Conditioning Processes



- i) Sensible heating \rightarrow $\begin{matrix} t \rightarrow \\ \text{DBT} \end{matrix}$ \rightarrow OA \rightarrow Temp increases only, no moisture added or removed ($w = \text{const}$)
- ii) Sensible cooling \rightarrow OB \rightarrow Temp (DBT) decreases only. no moisture added or removed. Hence w remains constant.
- iii) Humidifying and dehumidifying \rightarrow Only moisture content is added or decreased with no change in temp.
(OC) \rightarrow (OD)
- iv) Heating and humidifying \rightarrow OE \rightarrow As name suggests, both temperature and moisture content (w) is increased.
- v) Cooling and dehumidifying \rightarrow OF \rightarrow As name suggests, both temperature and moisture content of air (w) decreases.
- vi) Cooling and humidifying \rightarrow OG \rightarrow Temperature of air decreases but ~~but~~ moisture content (w) increases.
- vii) Heating and dehumidifying \rightarrow Temperature of air increases but moisture content decreases.

↳ Sensible heating and cooling



$Q_s = \text{Sensible heat transfer} = m_a (h_B - h_A)$
 if m_a ~~mass~~ circulation rate of dry air (kg/s) is known, ~~from~~ Q_s can be calculated from psychrometric chart.

Alternatively,

$$Q_s = m_a C_p (t_B - t_A)$$

$C_p \rightarrow$ humid ~~sp~~ specific heat

$$= Q_v \rho C_p (t_B - t_A)$$

$Q_v \rightarrow$ volume flow rate of air in m^3/s

Generally volume flow rate of air is given by C_{mm} (cubic meter per minute)

$$\therefore Q_s = \frac{C_{mm}}{60} \cdot \rho \cdot C_p (t_B - t_A)$$

Taking std values $\rho = (1.2) \text{ kg/m}^3$ dry air

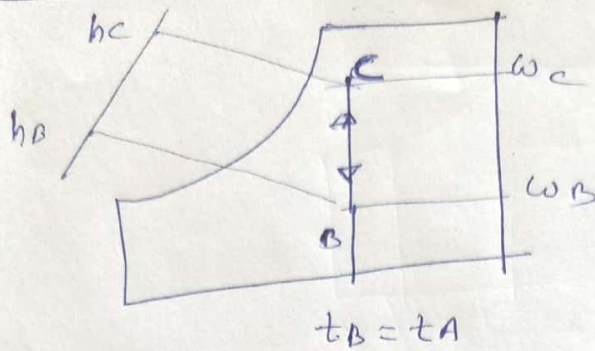
$C_p = 1.0216 \text{ kJ/kg.d.g. (K)}$

$$Q_s = \frac{C_{mm} \times 1.2 \times 1.0216 (t_B - t_A)}{60}$$

$$Q_s = \frac{0.0204 C_{mm} \Delta t}{1} \text{ kW}$$

Note: Simple cooling can be done only upto DPT (t_d)

② Latent Heat-Process (Humidifying or Dehumidifying)



Latent heat, $Q_L = m_a (h_c - h_b)$

can be calculated from psychrometric chart if m_a (kg of d.a./s) is known.

Alternatively

$$Q_L = m_a h_{fg0} (w_c - w_b)$$

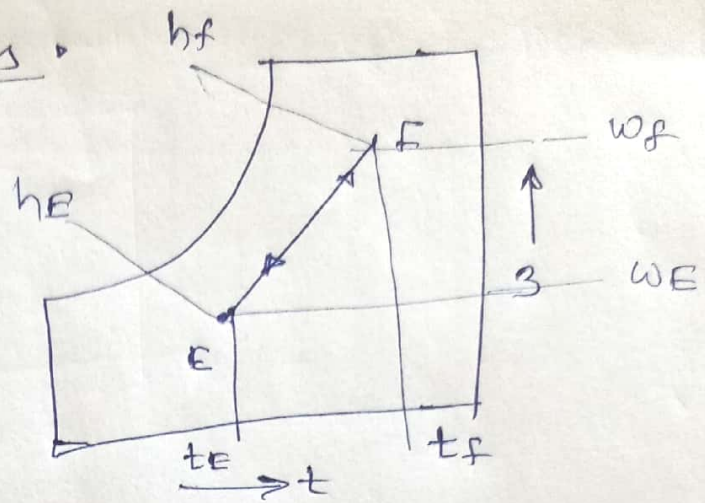
$h_{fg0} \rightarrow$ Latent-heat-of vaporization taken as 2500 kJ/kg

from previous section

$$m_a = \frac{(C \text{ mm}) \times 1.2}{60}$$

$$\begin{aligned} \therefore Q_L &= \frac{(C \text{ mm}) \times 1.2 \times 2500}{60} \Delta w \\ &= \underline{\underline{50 (C \text{ mm}) \Delta w \text{ kW}}} \end{aligned}$$

Total Heat Process



In this process as both temperature and humidity content changes, there is both sensible heat ^{load} change (Q_s) and latent heat load (Q_L) in the process

$$\therefore Q = Q_s + Q_L$$

Directly you can calculate it from psychrometric chart as $Q = m a (h_F - h_E)$

Alternatively

$$Q = \frac{Q_s}{c_{mm} \times 0.0204 \Delta t} + \frac{Q_L}{c_{mm} \times 50 \times \Delta w}$$

$$\therefore Q = c_{mm} (0.0204 \Delta t + 50 \times \Delta w)$$

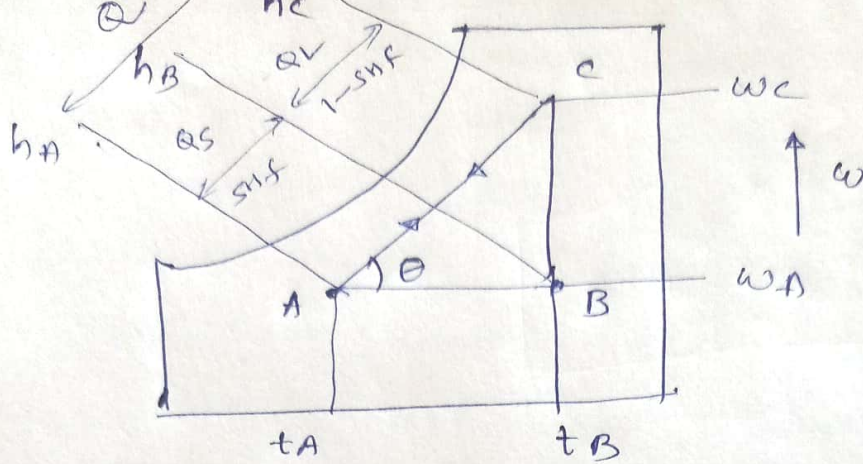
④ sensible heat factor (SHF)

Definition: The ratio of sensible Heat transfer to total heat transfer is called sensible heat transfer [Refer Above]

$$SHF = \frac{Q_s}{Q_s + Q_L} = \frac{Q_s}{Q}$$

~~SHF~~

Again drawing the process on psychrometric chart. (5)



Total heat = $h_c - h_A$ (per kg of dia)

sensible heat = $h_B - h_A$ (per kg of dia)

Latent heat = $h_c - h_B$

$$\therefore SHF = \frac{h_B - h_A}{h_c - h_A} = \frac{h_B - h_A}{(h_c - h_B) + (h_B - h_A)}$$

$$= \frac{0.0204 \Delta t}{0.0204 \Delta t + 50 \Delta w}$$

$$SHF = \frac{1}{1 + \frac{50 \Delta w}{0.0204 \Delta t}} = \frac{1}{1 + 2451 \tan \theta}$$

$$\frac{\Delta w}{\Delta t} = \tan \theta$$

from figure

The incoming moist air at point ① has temp t_1 and humidity content w_1 , it has dew point temp t_d . It means if the temp of air is lowered below t_d (or at least t_d), dew will be formed and moisture will get separated.

Now, the air is passed over the cooling coil which has temp t_s which is well below DPT (t_d) of entering air,

This temp (t_s) of cooling coil is called Apparatus Dew Point.

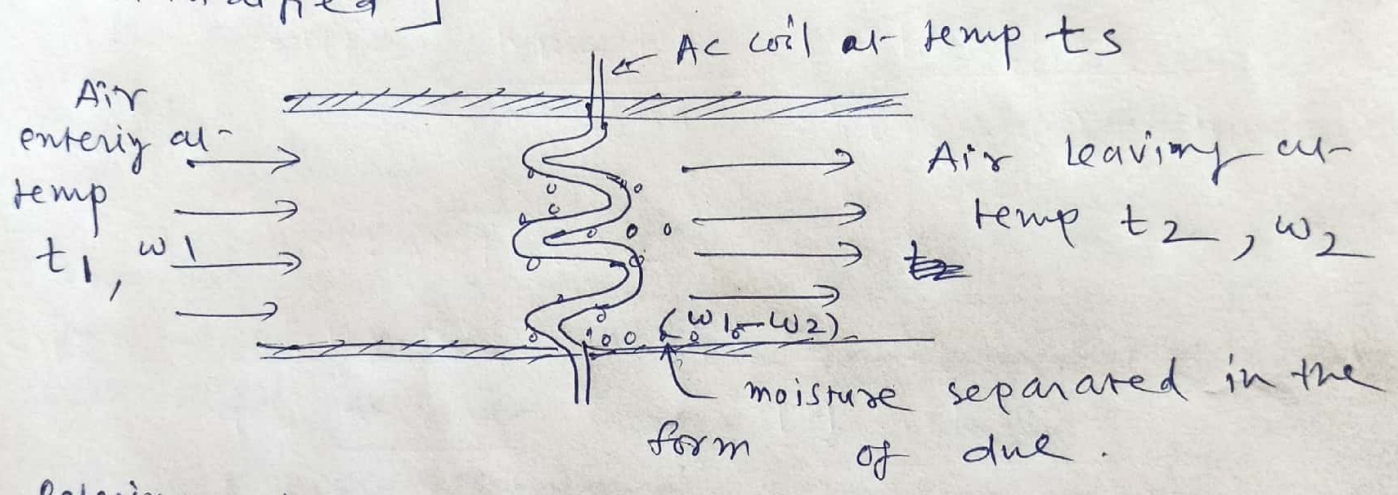
The air ~~is~~ leaves the coil at temp t_2 and at humidity w_2 . It means $(w_1 - w_2)$ moisture is removed from air.

Air is not cooled to lowest temp t_s (ADP). ~~It is viewed~~ The process is viewed as mixing of two parts of air. One part of air comes in contact with coil and cooled to temp t_s , other part does not come in contact and remain at temp t_1 . The final temp t_2 is the temp which is produced by mixing of this "contacted" and "uncontacted" air

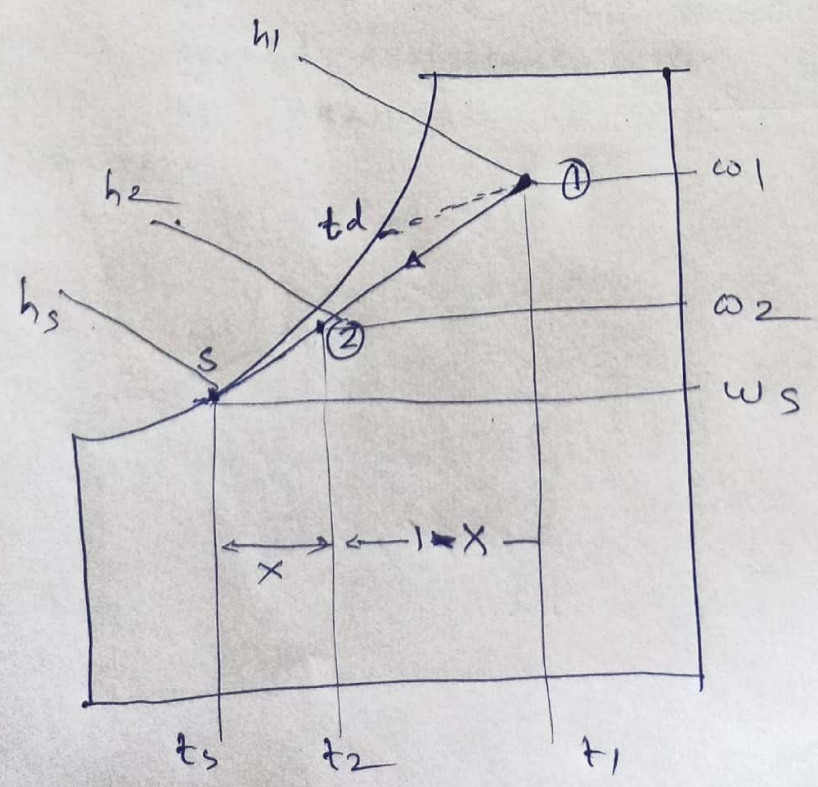
The bypass factor (BPF) of apparatus represent the fraction of this "uncontacted" air and denoted by X ,

* Bypan factor and Apparatus Dew Point (ADP)

Consider the air passing over cooling and dehumidifying coils as shown below.
 [It means refrigerant is passing ~~thru~~ inside coil which cools the entering air. Also the temperature of coil is kept below DPT (dew point-temp) of incoming air so that moisture in air get condensed and air leaves ~~cool~~ at coil, cool and dehumidified]



Referring to psychrometric process below



$$X = \frac{t_2 - t_s}{t_1 - t_s} = \frac{w_2 - w_s}{w_1 - w_s} = \frac{h_2 - h_s}{h_2 - h_1}$$

$(1-X)$ is called ~~to~~ contact factor

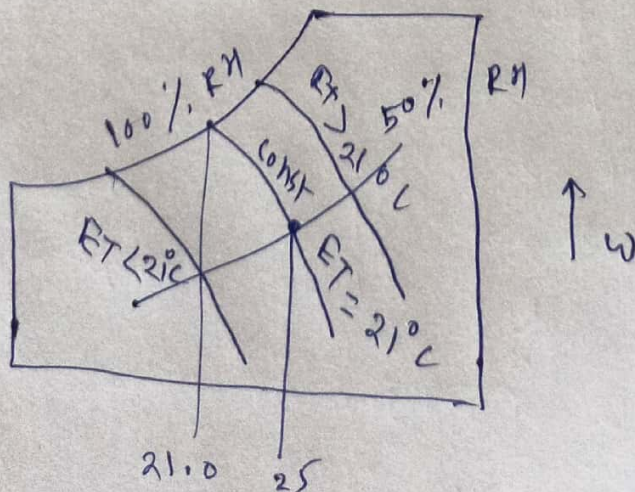
— X —

Comfort Air Conditioning and Effective Temperature (ET)

Human feel comfortable depending on
 ① Temperature ② Humidity ③ velocity
 of surrounding air. It is obvious that
 this feeling of comfort will be different
 for different people.

As there are different parameters to
 measure human comfort, often a single
 parameter called Effective Temperature (ET) is
 considered as an index of comfort.

Effective Temperature is defined as that
 temp of saturated air at which the subject
 (person) would experience the same feeling of
 comfort as measured in actual unsaturated
 environment.



There are variation in human comfort parameters depending on different study.

But ~~As~~ referring to ASHRAE chart

DBT = 20°C to 26°C

RH = 20% to 80%

are the ranges between which most human beings will feel comfortable

[You can refer to any good text book or material to draw comfort chart]

—X—